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## ADAPTIVE ANALOG EQUALIZER

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#### 1. Field of the Invention.

The present invention relates generally to analog equalization; and, more particularly, it relates to adaptive analog equalization

#### 2. Related Art.

Existing technologies for analog equalization commonly utilize the shape of a signal pulse to drive equalization adaptation for countering the undesirable channel attenuation and distortion. These conventional techniques are effective for most "return-to-zero" AMI line codes, but for DS3 or E3 line code applications, the pulse mask is spread to the point that it can essentially be considered non-return-to-zero within the bit period. In this case, it is difficult to train the equalizer when starting from either an over-equalized condition or an under-equalized condition.

Existing analog equalization techniques commonly trigger on the rising edge of a pulse and then sample the signal some time later at the falling edge where the sampled value is expected to be close to zero. The later sampling is typically about  $\frac{3}{4}$  of a symbol period later. The sampled value is an indication of the degree of over-equalization or under-equalization. This indication is used as the error term in the equalizer feedback control loop.

Fig. 1A is a system diagram illustrating an idealized adaptive analog equalization system 100A. The system in Fig. 1A is illustrative of the situation where equalization is performed at the receive end of a communication channel, somehow trying to compensate for the deleterious effects of intersymbol interference within the communication channel. An input signal 110A is passed through a communication channel 130A having a transfer function shown as  $H(s)$ . The communication channel 130A is terminated by an equalizer 142A having a transfer function  $[~1/H(s)]$  that is, ideally, the inverse of the transfer function of the communication channel 130A. The output signal 112A is, ideally, an exact duplicate of the input signal 110A.

Many conventional equalization systems operate using digital correction techniques. While these digital techniques are amenable to many applications, they are simply insufficient for very high frequency applications. As the operational frequencies continue to increase within various communication systems, the conventional digital correction techniques need similarly to increase in terms of operational frequency.

Further limitations and disadvantages of conventional and traditional systems will become apparent to one of skill in the art through comparison of such systems with the present invention as set forth in the remainder of the present application with reference to the drawings.

### SUMMARY

The present invention provides an adaptive analog equalizer that operates on a received input signal. The adaptive analog equalizer includes a high pass network and a multiplier that has an adjustable gain. The high pass network and the multiplier  
5 have a frequency response that, when adaptively applied to the input signal, are operable to compensate for corruption in the input signal. The output signal from the adaptive analog equalizer is used to drive the gain control through a feedback loop to adjust the adjustable gain of the multiplier. The received input signal is modified by the high pass network and the multiplier and is then summed with itself.

10 In one embodiment of the invention, the received input signal is a channel corrupted input signal. However, the adaptive analog equalizer is operable on the input signal when there is no corruption in the input signal as well without any additional complexity. When the input signal is provided from a communication channel, the frequency response of the adaptive analog equalizer is adapted to be  
15 substantially an inverse of the frequency response of the channel. The gain control performs decision and sampling control of the output signal from the adaptive analog equalizer, and feeds it back to the multiplier of the adaptive analog equalizer through an integrator. The adaptive analog equalizer requires variable gain amplification, to be performed on its input signal. The variable gain amplifier in conjunction with an  
20 integrator, and a peak detector is employed for this purpose. The output signal from the adaptive analog equalizer is processed through the peak detector and the integrator to provide a feedback control signal for the variable gain amplifier. The decision and sampling control block in the gain control circuit is operable to perform double

sampling of its input signal. The decision and sampling control circuit waits a first predetermined period of time after pulse rising edge detection before sampling a first sample of the input signal. In addition, it waits a second predetermined period of time after pulse rising edge detection before sampling a second sample of the input signal.

5        Other features of the present invention can be found in a double sampling adaptive analog equalizer. The double sampling adaptive analog equalizer includes a decision and sampling control block inside a gain control unit that is operable to perform double sampling of an input signal. The gain-control processed feedback loop forces the input signal to a predetermined value within  $3/4^{\text{th}}$  of a bit period after  
10    detecting a rising edge. The predetermined value to which the input signal is forced is zero.

In some embodiments of the invention, the decision and sampling control waits a first predetermined period of time before sampling a first sample of its input signal. In one embodiment, the first predetermined period of time is less than a pulse  
15    period. In addition, the decision and sampling control waits a second predetermined period of time before sampling a second sample of the input signal. In one embodiment, the second predetermined period of time is greater than a pulse period.

The adaptive analog equalizer structure of the present invention also includes a high pass network and a multiplier having an adjustable gain. The input signal is  
20    provided from a communication channel having a channel frequency response, and a frequency response of the high pass network and the multiplier is substantially an inverse of the channel frequency response.

Other aspects of the present invention can be found in a method to perform analog adaptive equalization. The method involves detecting a rising edge of an input signal, waiting a first predetermined period of time before sampling a first sample of the input signal, waiting a second predetermined period of time before sampling a  
5 second sample of the input signal, and adjusting a gain of a multiplier when the second sample does not exceed a predetermined threshold.

In some embodiments of the invention, the first predetermined period of time is less than a pulse period. The second predetermined period of time is greater than a pulse period. The input signal is a channel corrupted input signal. The method also  
10 involves forcing the input signal to zero within  $3/4^{\text{th}}$  of a bit period in response to a one to zero transition.

Other systems, methods, features and advantages of the invention will be or will become apparent to one with skill in the art upon examination of the following figures and detailed description. It is intended that all such additional systems,  
15 methods, features and advantages be included within this description, be within the scope of the invention, and be protected by the accompanying claims.

**BRIEF DESCRIPTION OF THE DRAWINGS**

The components in the figures are not necessarily to scale, emphasis instead being placed upon illustrating the principles of the invention. In the figures, like reference numerals designate corresponding parts throughout the different views.

5        Fig. 1B is a system diagram illustrating an embodiment of an actual adaptive analog equalization system designed in accordance with the present invention.

Fig. 2A is a flow diagram illustrating an embodiment of received signal flow within an adaptive analog equalization system operating in accordance with the present invention.

10       Fig. 2B is a system diagram illustrating an embodiment of an adaptive analog equalizer structure built in accordance with the present invention.

Fig. 3 is a timing diagram illustrating adaptive analog equalizer transition correction performed in accordance with the present invention.

15       Fig. 4 is a functional block diagram illustrating an embodiment of an adaptive analog equalizer method performed in accordance with the present invention.

Fig. 5 is a functional block diagram illustrating another embodiment of an adaptive analog equalizer method performed in accordance with the present invention.

Fig. 6 is a timing diagram illustrating an isolated 0/1/0 pattern that is properly corrected using adaptive analog equalization in accordance with the present invention.

20       Fig. 7 is a timing diagram illustrating an isolated 0/1/1 pattern that is properly processed using adaptive analog equalization in accordance with the present invention.

### DETAILED DESCRIPTION

Fig. 1B is a system diagram illustrating an embodiment of an actual adaptive analog equalization system 100 designed in accordance with the present invention. A transmitter 120 generates an input signal 110 that is passed through a communication channel 130 having a transfer function shown as  $H(s)$ . The input signal 110 is then transformed into a channel corrupted output signal 111. The channel corrupted output signal 111 is then passed to a receiver 140. The receiver 140 employs an adaptive equalization circuitry 142 having a transfer function  $[~1/H(s)]$  that is substantially close to the inverse of the transfer function of the communication channel 130. The corrected output signal 112 is then substantially similar to the input signal 110A.

Fig. 2A is a flow diagram illustrating an embodiment of received signal flow 200 within an adaptive analog equalization system operating in accordance with the present invention. The received signal flow 200 shows an input signal that is provided to a communication channel 210 having a transfer function shown as  $H(s)$ . The communication channel 210 is viewed as being essentially a low pass network. Output from the communication channel 210 is a channel corrupted input signal that is provided to a variable gain amplifier (VGA) 220. The VGA 220 is communicatively coupled to an adaptive analog equalizer structure 230 that is itself communicatively coupled to a slicer 260. The output from the slicer 260 is shown as the output signal.

The output of the adaptive analog equalizer structure 230 is fed back through two distinct feedback control loops. One of the control loops is where the output of the adaptive analog equalizer structure 230 is fed to a peak detector 240 that provides

an output to an integrator 250. The integrator 250 provides an output to a VGA 220. The other of the control loops is where the output of the adaptive analog equalizer structure 230 is fed to a gain control block 270. The gain control block 270 includes a decision/sampling control block 272 and an integrator 274. The output of the gain control block 270 is fed to the adaptive analog equalizer structure 230.

The received signal flow 200 shows double sampling of the output of the adaptive analog equalizer structure 230 performed in accordance with the present invention. Two distinct samples are taken after the rising edge trigger of the signal. The first sample is operable to measure the error term. If desired, the first sample is nominally taken at  $3/4^{\text{th}}$  symbol period after the trigger. The second sample is operable to determine a one-zero (1/0) transition. If desired, the second sample is taken nominally at  $1 \text{ and } 1/4^{\text{th}}$  symbol periods after the trigger. The error term is used if a one-zero (1/0) transition is detected.

The present invention is operable to ensure that the equalizer will converge regardless of the initial conditions of the adaptation. As mentioned above, the present invention is particularly effective within DS3 or E3 line codes, but it is operable for any RZ pulse or on-off keying signal.

Fig. 2B is a system diagram illustrating an embodiment of an adaptive analog equalizer structure 230 built in accordance with the present invention. In many respects, the adaptive analog equalizer structure 230 can be viewed as being the adaptive analog equalizer structure 230 of the Fig. 2A.

The adaptive analog equalizer structure 230 of the Fig. 2B includes an adaptive equalization circuitry 232 that is operable on an input signal. Using a gain



control input, the input signal is modified and transformed into an output signal. The adaptive equalization circuitry 232 includes a high pass network (HP N/W) 234, an amplifier having a gain 236 and a summing junction. The adaptive equalization circuitry 232 has a transfer function that is essentially the inverse of a communication  
5 channel from which the input signal is provided.

The input signal is provided to the high pass network (HP N/W) 234 within the adaptive equalization circuitry 232 and also to the summing junction within the adaptive equalization circuitry 232. The output from the high pass network (HP N/W) 234 is passed to the amplifier having a gain 236. The gain 236 is adaptable as a  
10 function of the gain control. From certain perspectives, the gain control of the adaptive analog equalizer structure 230 is viewed as being the gain control 270 of the Fig. 2A.

Fig. 3 is a timing diagram illustrating adaptive analog equalizer transition correction 300 performed in accordance with the present invention. An ideal one to  
15 zero ("1" to "0") transition 305 shows a value of signal transitioning from a high value to a low value precisely at the junction between two nominal bit periods. However, an actual (smeared) one to zero ("1" to "0") transition 315 where the signal transitions from a high value to a low value over multiple bit periods. The " $\Delta t$ " nominally shows a period during which the signal transition, if it were completely  
20 performed, would cause no problems and require no equalization correction. However, there is a problematic region 335 during which it is unclear, from a signal processing perspective, whether there has or has not been an actual transition. The problem arises when a one to zero ("1" to "0") transition has not been fully

accomplished and the next nominal bit period has a non-zero signal level, resulting in the slicer interpreting the bit as a 1 instead of a 0. The adaptive analog equalizer corrected one to zero ("1" to "0") transition 325 shows where the signal level is forced to zero "0" 345 within one nominal bit period. The problematic region 335 is  
5 existent within conventional adaptive analog equalization systems.

Fig. 4 is a functional block diagram illustrating an embodiment of an adaptive analog equalizer method 400 performed in accordance with the present invention. In a block 410, dual sampling is performed. Then, in a decision block 420, it is determined whether a pulse to no pulse (1/0) transition has been detected. If yes, then  
10 adaptation control is performed in a block 430. An equalizer structure is employed as shown in a block 435 when performing the adaptation control in the block 430. The equalizer structure employed in the block 435 is the adaptive analog equalizer structure 230 shown in the Figures 2A and 2B. If no, the adaptive analog equalizer method 400 continues back to the block 410.

15 Fig. 5 is a functional block diagram illustrating another embodiment of an adaptive analog equalizer method 500 performed in accordance with the present invention. In a decision block 510, it is determined whether a pulse rising edge is detected. If no, then the adaptive analog equalizer method 500 returns to the decision block 510. If a rising edge is detected as determined in the decision block 510, then  
20 two different paths are taken as shown by a block 520 and a block 525.

In the block 520, the adaptive analog equalizer method 500 waits a predetermined amount of time. If desired in alternative embodiments, the time that is waited is  $\frac{3}{4}$  of a nominal pulse period as shown in an alternative block 521. Then, a

pulse is sampled as shown in a block 530. The value "s1" is shown as being the sample in the block 530. Then, an "enableOn pulse to no pulse" transition is made in a block 540.

In addition, in the block 525, the adaptive analog equalizer method 500 also  
5 waits a predetermined amount of time. If desired in alternative embodiments, the time that is waited is  $1\frac{1}{4}$  of a nominal pulse period as shown in an alternative block 526. The predetermined time period extends into the next pulse as shown in the alternative block 526. Then, the next pulse is sampled as shown in a block 535. The value "s2" is shown as being the sample of the next pulse in the block 535. The  
10 sample "s2" is the absolute value of the next pulse as shown in the block 535. Then, in a decision block 545, it is determined if the sample "s2" is less than or equal to a predetermined threshold "thresh2." If no, then the adaptive analog equalizer method 500 begins and returns to the decision block 510. However, if it is determined if the sample "s2" is less than or equal to a predetermined threshold "thresh2," then it is  
15 concluded that a pulse to no pulse (1/0) transition has taken place and the adaptive analog equalizer method 500 continues to the "enableOn pulse to no pulse" transition as shown in the block 540. The "yes" decision derived from the decision block 545, feeding into the block 540, serves as a trigger to proceed to a block 550.

Subsequent to the operation in the block 540, an integrator operates on the  
20 sample "s1" as shown in the block 550. Then, an equalizer is adapted and the equalizer gain is adjusted in the block 560. The equalizer gain is that adjusted in the block 560 is the amplifier having the gain 236 in the Fig. 2B. The gain control that

performs the equalizer gain adjust in the block 560 is the gain control block 270 as shown in the Fig. 2A above.

Fig. 6 is a timing diagram illustrating an isolated 0/1/0 pattern 600 that is properly corrected using adaptive analog equalization in accordance with the present invention. Pulse rising edge detection is performed on the isolated 0/1/0 pattern 600. There are three different types of equalization performed in the Fig. 6. For each of the three cases, a first sample "s1" and a second sample "s2" are made near the transition of the isolated 0/1/0 pattern 600. For an over-equalized signal, the first sample "s1" and the second sample "s2" are both negative. For both the under-equalized signal, the first sample "s1" and the second sample "s2" are both positive. For the properly equalized signal, resulting from the analog adaptive equalization performed in accordance with the present invention, both the first sample "s1" and the second sample "s2" are properly aligned close to the zero axis after performing the transition of the isolated 0/1/0 pattern 600 as shown by the solid line.

Fig. 7 is a timing diagram illustrating an isolated 0/1/1 pattern 700 that is properly processed using adaptive analog equalization in accordance with the present invention. A false detection of a pulse edge is performed in those situations where over-equalization and under-equalization are performed using conventional equalization techniques.

For the properly equalized signal, resulting from the analog adaptive equalization performed in accordance with the present invention, the isolated 0/1/1 pattern 700 is shown as the solid line.

While various embodiments of the invention have been described, it will be apparent to those of ordinary skill in the art that many more embodiments and implementations are possible that are within the scope of this invention.